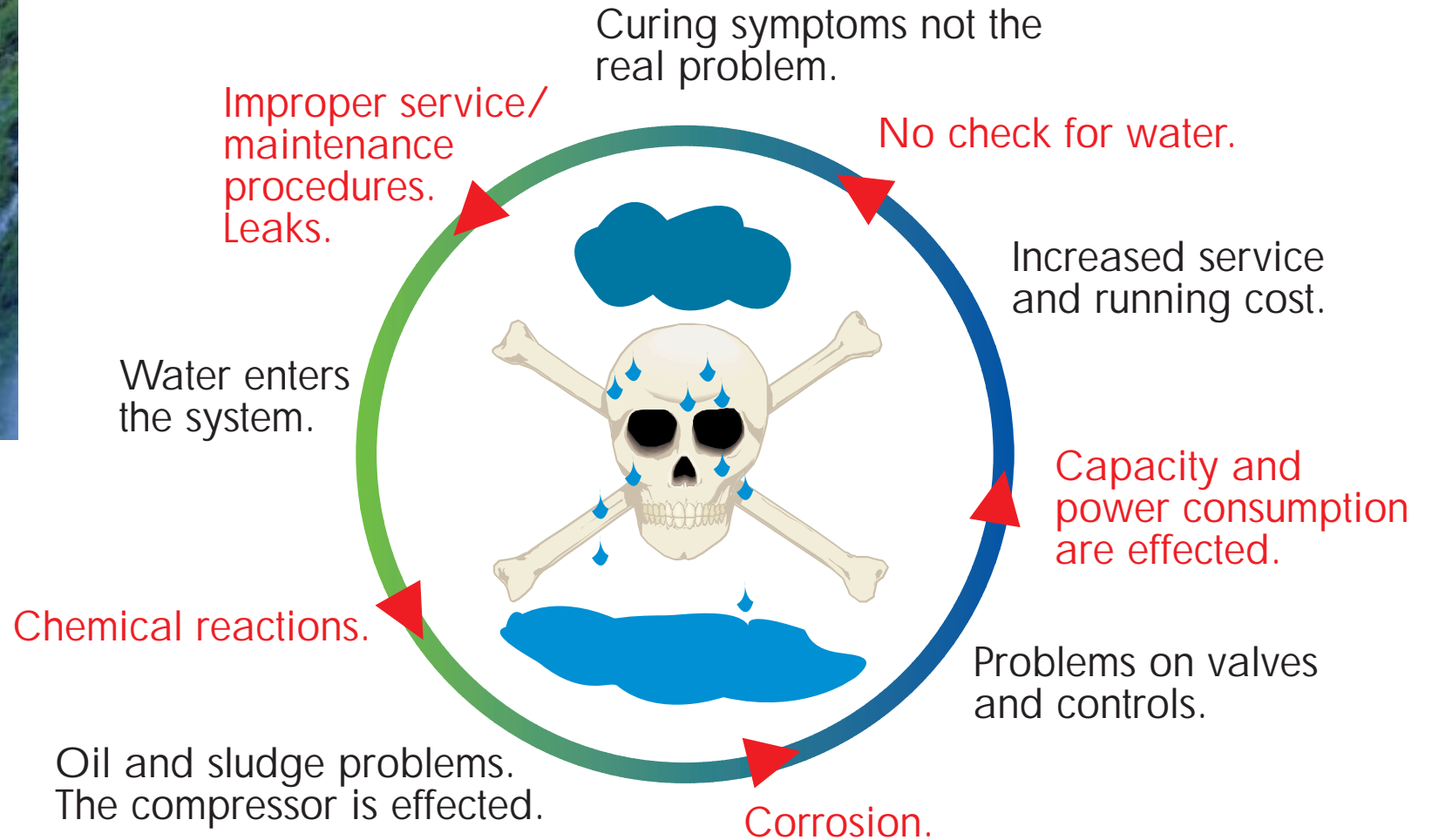
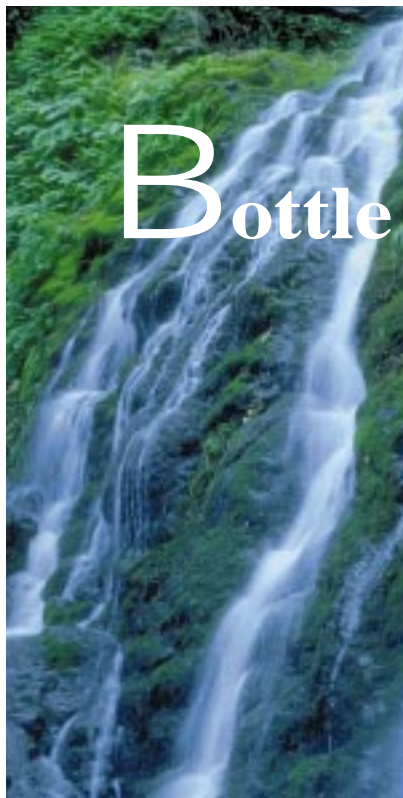


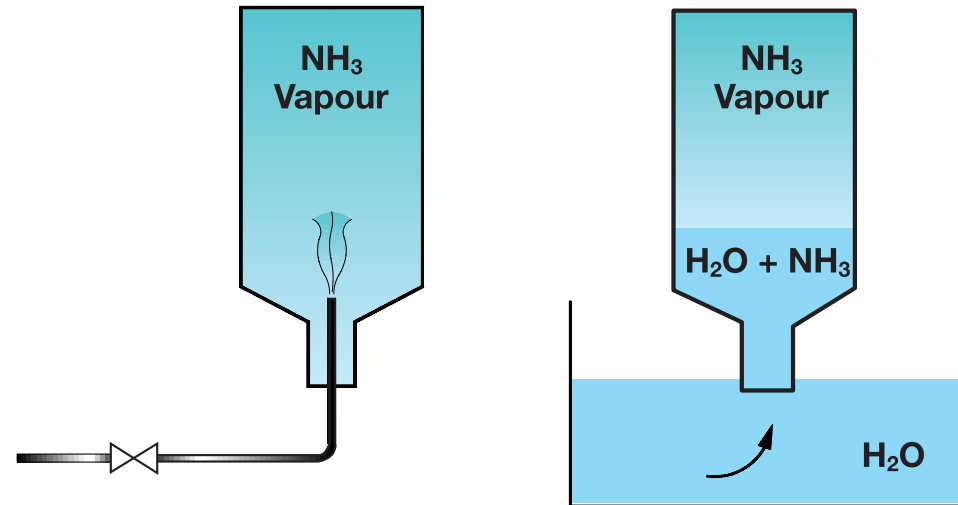
Effects of water contamination “The evil circle”



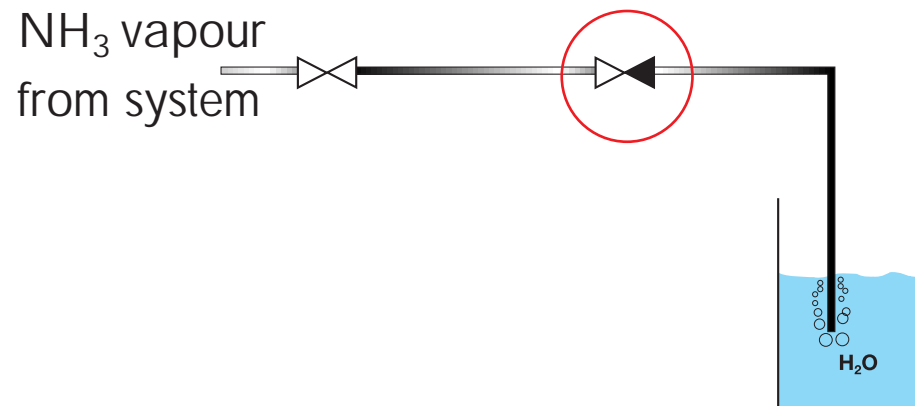


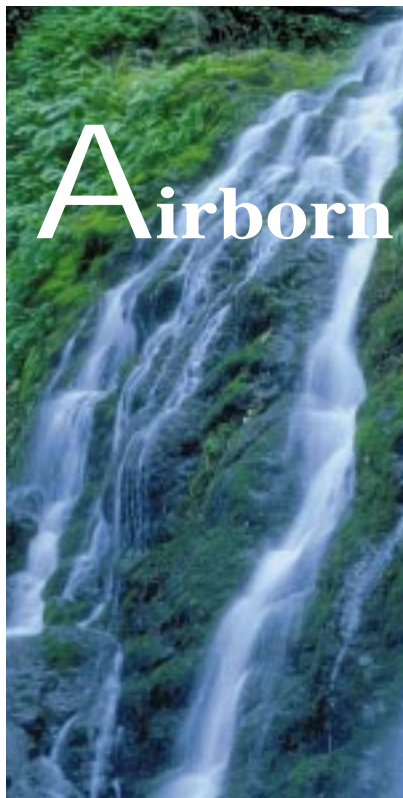
Bottle test

- shows the affinity between NH_3 and H_2O



Always use a checkvalve, when evacuating through water





Airborn moisture

Max. capacity for an airpurger is approx. 10 l/min. (at atm. press.)

Imagining "Worst Case":

Purging 5 l/min. air continuously.

Ambient temperature 20°C (43,1 F). Humidity 80%.

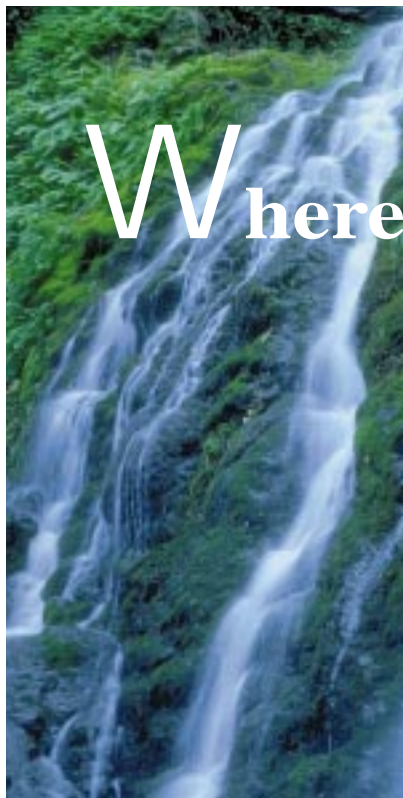
This means:

- ▶ 4.15 g H₂O enters the system each hour.
- ▶ 36.35 litres each year.
- ▶ 363.5 litres H₂O after 10 years.

After 10 years:

363.5 kg \approx 6058 l NH₃ charge have 10% H₂O content.

181.8 kg \approx 3029 l NH₃ charge have 20% H₂O content.



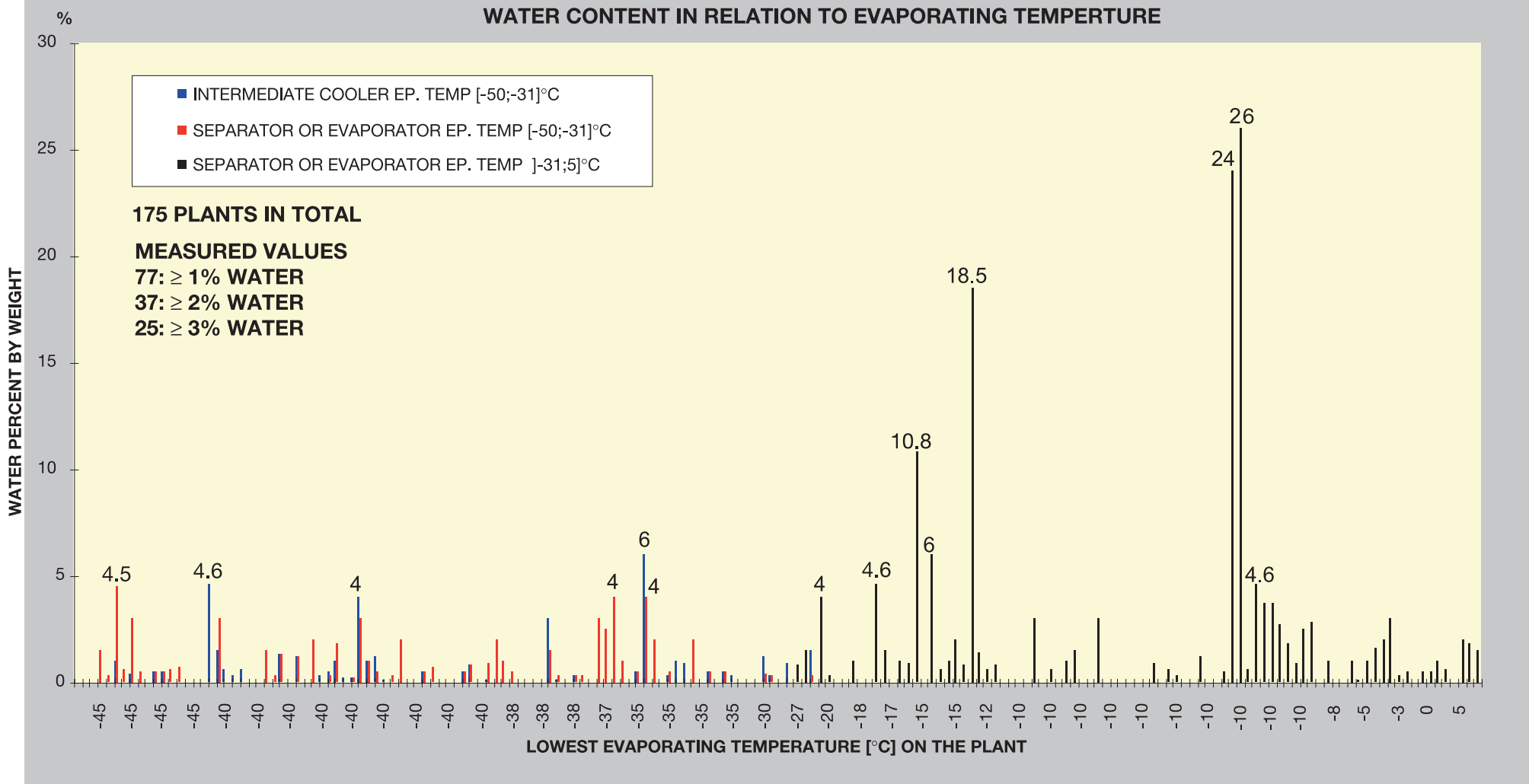
Where the water goes in the system depends on the design

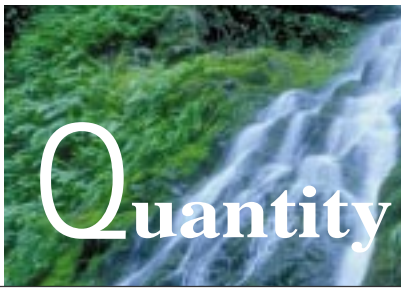
- ▶ **Flooded systems with efficient liquid separators:**
H₂O stays on LP side and EP side
(separators/evaporators, intermediate coolers).
Liquid carry over ⇒ high amounts of H₂O can go to compressors.
- ▶ **Systems where defrost drainlines goes to HP side:**
H₂O will be carried to everywhere in the system.
Dangerous for compressors with liquid injection, dry expansion economizers and intermediate cooling.
- ▶ **Dry expansion systems:**
H₂O is carried with high velocity suction gas to the separator/
compressor.

NOTE: Thermostatic expansion valves will react on the change in saturated temp. for NH₃ + H₂O as “superheat” and might be unable to control the evaporator.

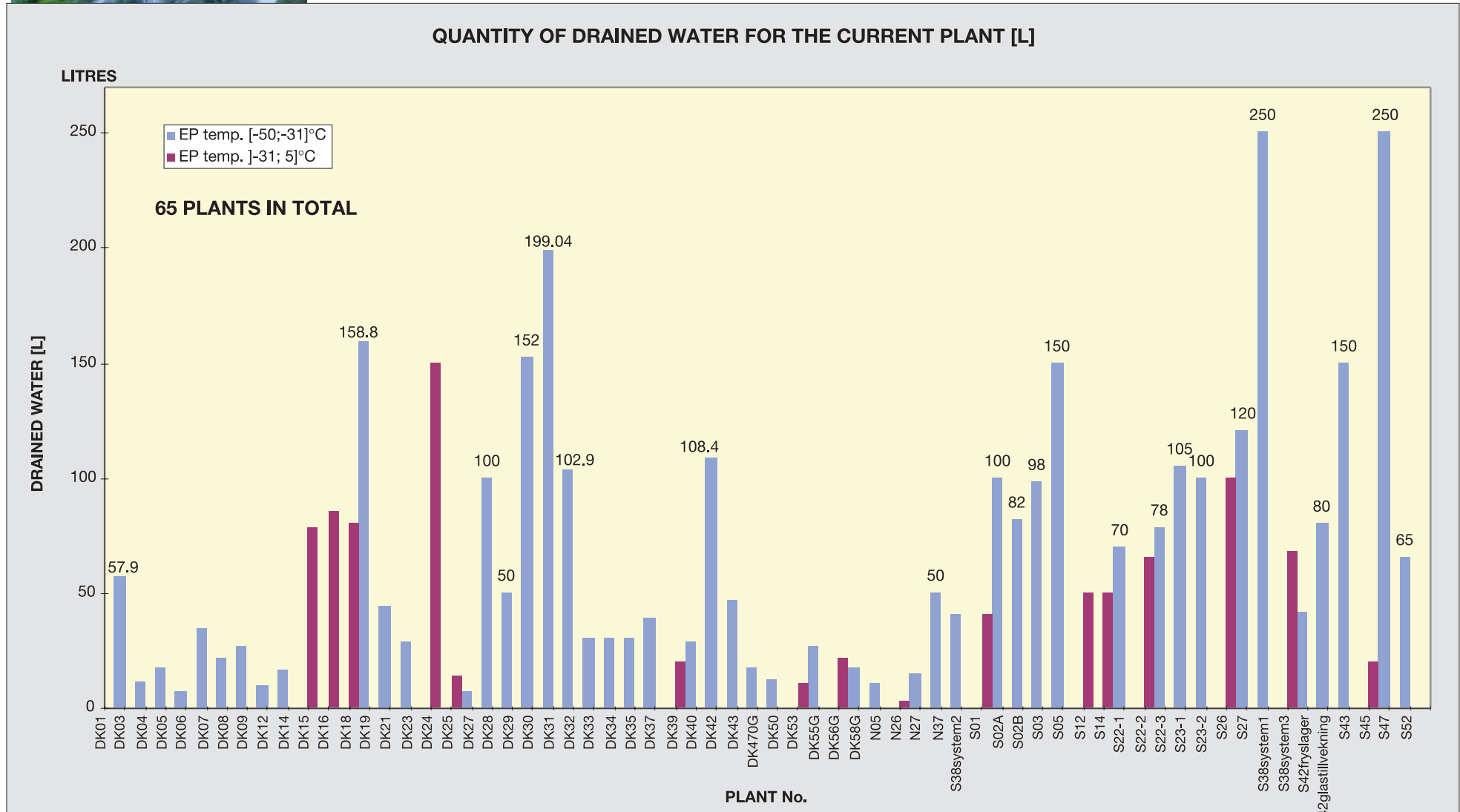


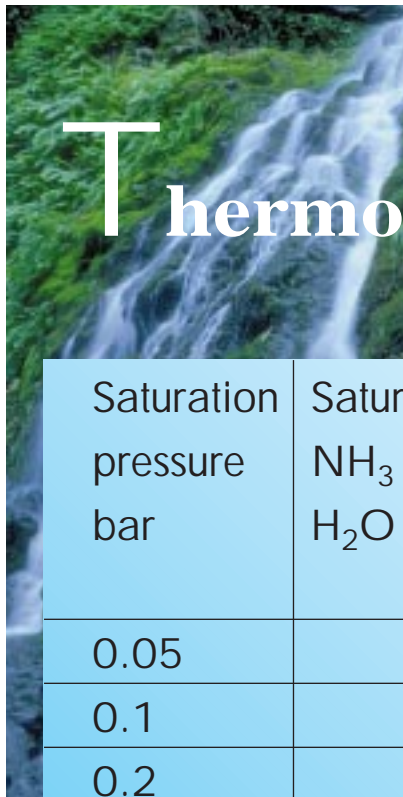
Water content in relation to evaporating temp.





Quantity of drained water for the current system [L]

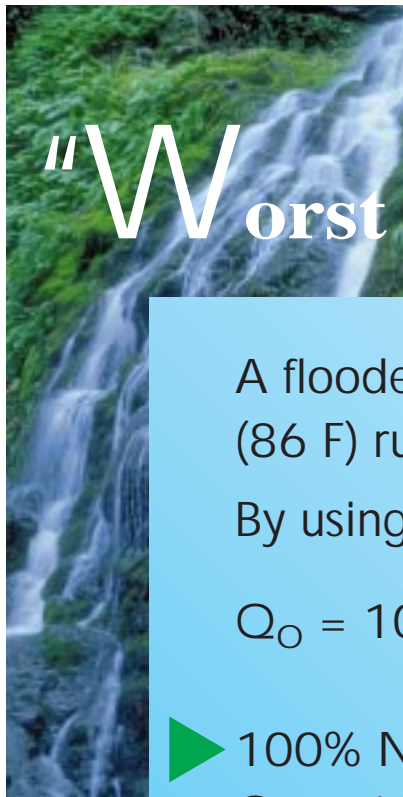




T hermodynamic properties NH₃ + H₂O

Saturation pressure bar	Saturation temperature, °C if				
	NH ₃	70%	80%	90%	100%
	H ₂ O	30%	20%	10%	0%
0.05	NA	NA	NA	NA	NA
0.1	NA	NA	NA	NA	NA
0.2	NA	NA	NA	NA	NA
0.3	-47.15	NA	NA	NA	NA
0.4	-42.10	-46.48	-48.82	NA	NA
0.5	-38.00	-42.51	-44.93	-46.52	NA
1.0	-24.07	-28.96	-31.71	-33.59	NA
2.0	-7.71	-13.63	-16.70	-18.85	NA
3.0	2.51	-3.16	-6.69	-9.23	NA
4.0	10.32	4.45	0.79	-1.88	NA

Saturation temp. °C	Saturation pressure, bar if				
	NH ₃	70%	80%	90%	100%
	H ₂ O	30%	20%	10%	0%
-50	0.254	0.326	0.373	0.408	NA
-48	0.285	0.366	0.420	0.459	NA
-46	0.321	0.411	0.471	0.515	NA
-44	0.360	0.460	0.527	0.576	NA
-42	0.402	0.514	0.588	0.644	NA
-40	0.449	0.573	0.655	0.717	NA
-38	0.500	0.637	0.728	0.797	NA
-36	0.556	0.708	0.808	0.885	NA
-34	0.617	0.784	0.895	0.980	NA
-32	0.679	0.861	0.986	1.08	NA



"Worst case" calculation example

A flooded system with screw compressors at $ET = -42^{\circ}\text{C}$ (-43.6 F) , $CT = 30^{\circ}\text{C}$ (86 F) runs 10 hours/day 300 days a year.

By using $\text{COP} = \frac{Q_O}{N_E}$, what is the power consumption (N_E) each

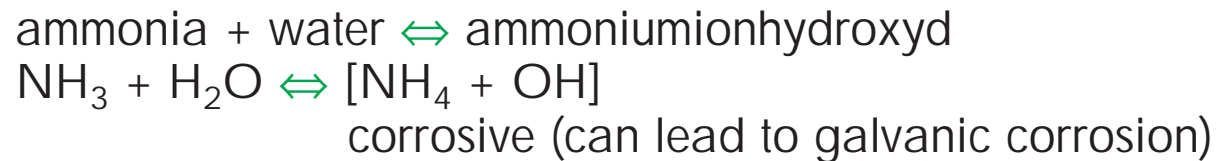
$Q_O = 1000\text{ kW}$ (284 TR)/year

- ▶ 100% NH_3 : EP = 0.64 bar a (9.28 psia) $Q_O = 361.7\text{ kW}$ (102.7 TR)
 $Q_O = 1000\text{ kW}$ (284 TR) $\Rightarrow N_E = 2097900\text{ kWh/year}$.
- ▶ 90% NH_3 + 10% H_2O : EP = 0.59 bar a (8.56 psia) $Q_O = 327.1\text{ kW}$ (92.9 TR)
 $Q_O = 1000\text{ kW}$ (284 TR) $\Rightarrow N_E = 2272800\text{ kWh/year} \Rightarrow$
 additional $N_E = 174900\text{ kWh/year}$ each $Q_O = 1000\text{ kW}$.
- ▶ 80% NH_3 + 20% H_2O : EP = 0.51 bar a (7.40 psia) $Q_O = 278.8\text{ kW}$ (79.2 TR)
 $Q_O = 1000\text{ kW}$ (284 TR) $\Rightarrow N_E = 2586300\text{ kWh/year} \Rightarrow$
 additional $N_E = 488400\text{ kWh/year}$ each $Q_O = 1000\text{ kW}$ (284 TR)



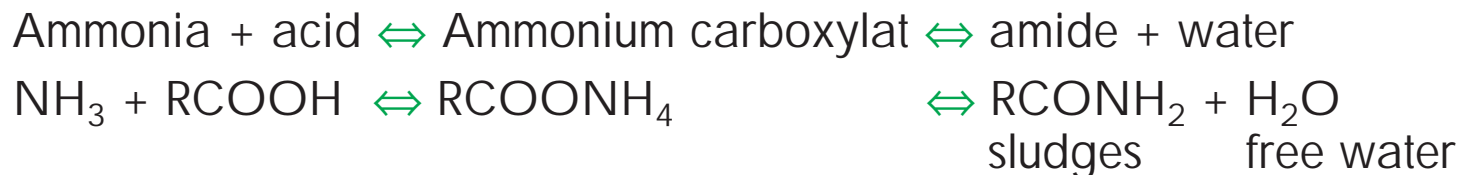
Pure anhydrous ammonia is not very chemical reactive

- ▶ "Wet" ammonia form the very chemical reactive:

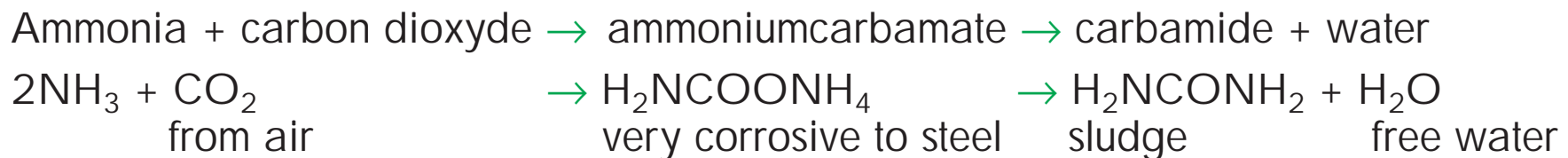


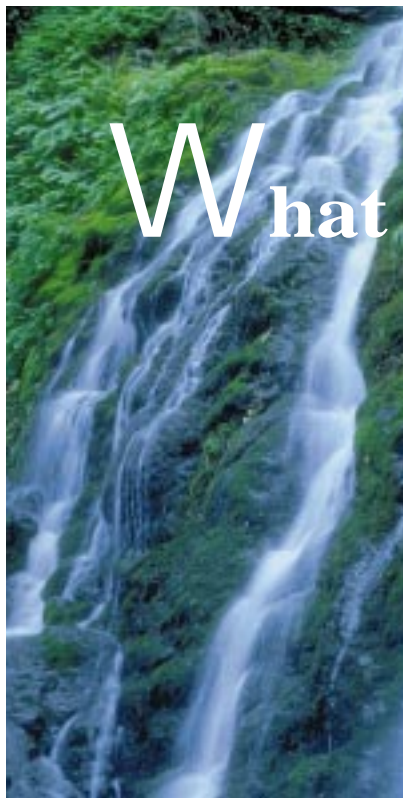
Water can be created in the system

- ▶ Reaction with acid from oxydation of oil.



- ▶ Air in the system will allow following reaction:





What happens to the oil?

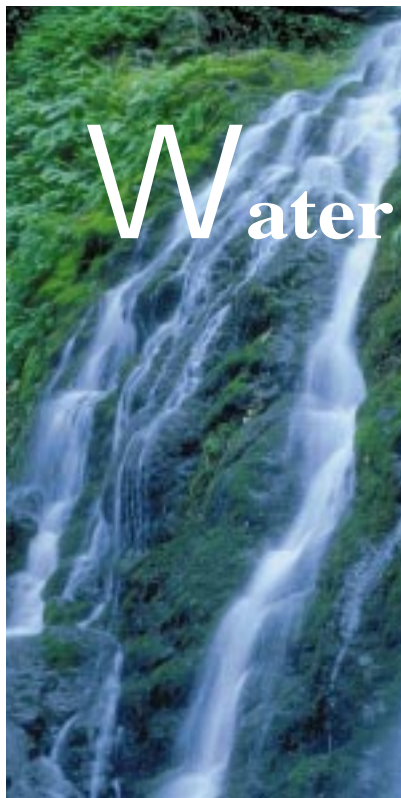
Oxydation: Oil + oxygen + water \Rightarrow precursors + organic acids.

Nitriding: Oil + ammonia + water \Rightarrow precursors + organic acids

Organic acid + ammonia \Rightarrow nitro compounds
(sludges, salts, soap products).

Nitro compounds:

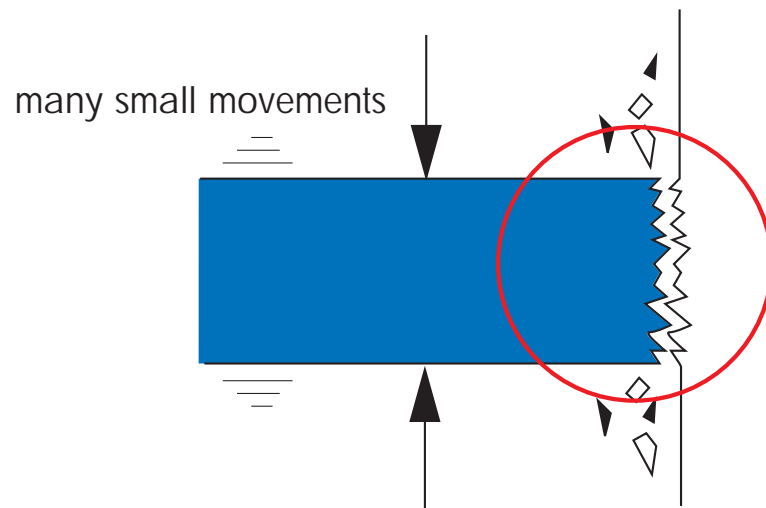
- ▶ are partly soluble in ammonia.
- ▶ are not soluble in oil.
- ▶ can escape through oilseparators.
- ▶ makes sludges in the compressors and in the system (valves, controls, evaporators etc.).
- ▶ acts as catalysist and are amplifying the process of creating more nitro compounds.

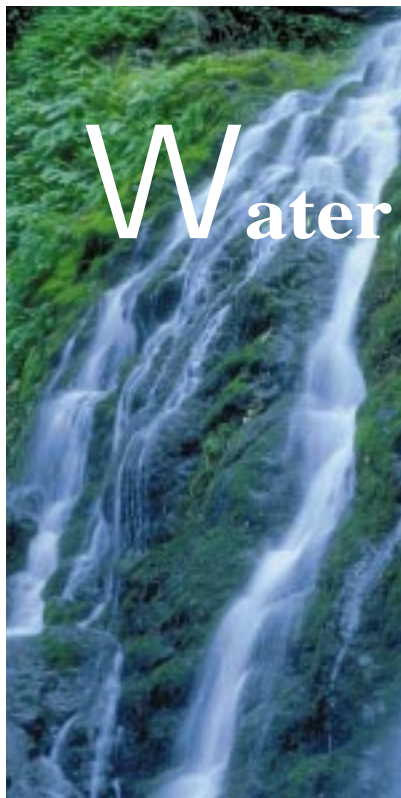


Water related problems on valves and controls

▶ **Rust and sludges:** Valves, filters can get “clogged” or stock.

▶ **Fretting corrosion:** Vibrations/pulsations ⇒
 fatigue in asperities ⇒
 asperities brake off ⇒
 free particles on surfaces + corrosion ⇒
 particles “grow” in size ⇒
 increased friction ⇒
 more wear ⇒
 valves/controls can get “stock”





Water related problems in expansion devices

- ▶ Highly increased wear problems in expansion devices.

Possible reasons (not proven):

Increased erosion because of high amount of dirt particles.

Collaps of water vapour into small drops with a cavitation effect.

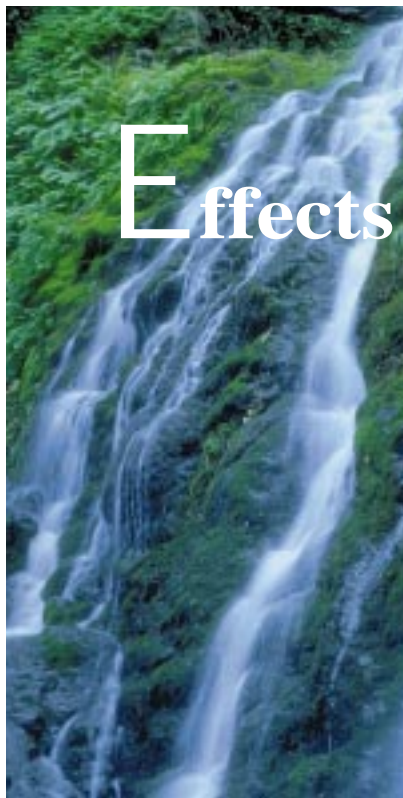
Introducing corrosion with the erosion and cavitation.

- ▶ Thermostatic expansion valves might not operate correctly due to changes in saturated liquid temp. for $\text{NH}_3 + \text{H}_2\text{O}$



Conclusions on water contamination

- ▶ NH₃ systems often contain more water than recommended.
- ▶ Proper procedures in service work plays an important role.
- ▶ Automatic airpurgers can “hide” leak problems.
- ▶ System design is important for water related problems.
- ▶ Water related problems are not very well-known to system operators and service staff.
- ▶ Detection of water contamination should be carried out as part of normal service and maintenance (Ilar Bulletin No. 108).
- ▶ Installation of water rectifiers can prove to be a very attractive investment (Ilar Bulletin No. 108).



Effects of keeping systems dry

“The good dry circle”

